

Tunable Monopole Circular Microstrip Antenna for Wide FIBW covering Low frequency wireless applications

Biradar Rajendra^{1*}, S. N. Mulgi²

^{1,2}Dept. of Post Graduate Studies and Research in Applied Electronics, Gulbarga University, Kalaburagi – 585106 Karnataka, India

*Corresponding Author: biradarrajendra1864@gmail.com, Tel.: +91 9449140205

DOI: <https://doi.org/10.26438/ijcse/v7i5.12321236> | Available online at: www.ijcseonline.org

Accepted: 26/May/2019, Published: 31/May/2019

Abstract— In this paper, we have presented simulated and measured results of tunable monopole circular microstrip antenna for wide frequency impedance bandwidth which covers low frequency wireless applications. The proposed antenna consists of two identical slots placed on either side of feed axis having fixed dimensions of $L_1=0.446$ cm, $L_2=0.6$ cm and width $W_1=0.4$ cm. A stub of fixed width is loaded on left side of patch having with $W_s=0.9$ cm. The upper and lower length of stub is varied from $L_{US}=0.62$ to 1.22 cm and $L_{LS}=0.457$ to 1.057 cm to tune an antenna for wide frequency impedance bandwidth from 1.7425 GHz to 1.4725 GHz. This variation also increases the impedance bandwidth from 163 to 200% when simulated where as it varies from 98.6 to 164% when measured and gives a peak gain of 1.9079 dB. The proposed antenna can cover all low frequency microwave applications like GPS, GSM, DCS, PCS, UMTE, LTE, Wi-Fi, WLAN, Wi-MAX, FCC ID etc., The simulated results are in good agreement with experimental results. The VSWR is less than 2 . The radiation patterns are nearly Omni directional nature both in E and H plane.

Keywords— Identical slots, stub, TMCMSAWB and FIBW

I. INTRODUCTION

The microstrip antennas are more popular due to their inherent properties like low cost, easy to operate, easy to fabricate, Omni directional radiation pattern etc. However, there are some disadvantages such as narrow impedance bandwidth, low gain, poor radiation characteristics etc. [1-4]. In spite of limitations of microstrip antennas, in the recent wireless communications, they are of more useful for many applications. The tunable antennas with wide band width are more useful in many modern wireless communication systems in which optimum use of frequency spectrum is possible to use. Hence it is necessary to design tunable antennas for realizing the tunability for wide impedance band width. In this regard, there are numerous methods are proposed in the literature to enhance the impedance bandwidth with tunable property of microstrip antenna, like increasing the thickness of the substrate, decreasing dielectric constant of the substrate, using parasitic patches in single layer and multi layers configuration, employing electromagnetic band gap structures, using backed edge-fed cavity etc. All these are made by adding additional structure so that, the antenna geometry become more complex and bulky. The antennas of wider bandwidth and tunable properties are available in the literature designed separately, but a single antenna possessing both the properties are very

rarely found in the literature. This property of an antenna helps in using antenna for the desired band of frequency assigned for a specific application. Therefore, in the proposed study, the antenna is designed using a simple conventional method of slot and stub loading technique on a radiating patch. This technique also helps in widening the impedance bandwidth and shows the property of tuning. The impedance bandwidth increases when we increase the length of the stub where as it decreases inversely with frequency. The impedance bandwidth is increased up to 200% in this study. The single band property of an antenna also avoids interference between the nearby operating bands as in case of the multiband property of an antenna [5-11]. The proposed antenna gives a peak gain of 1.9079 dB in its operating band and shows Omni directional radiation properties in both E and H plane. This antenna can cover all low frequency microwave applications like GPS, GSM, DCS, PCS, UMTE, LTE, Wi-Fi, WLAN, Wi-MAX, FCC ID Etc., The experimental variation of return loss versus frequency of proposed antenna is in good agreement with the simulated results.

II. DESCRIPTION OF ANTENNA GEOMETRY

The conventional monopole circular microstrip antenna (CMCMSA) is designed using low cost modified glass epoxy of thickness $h=1.6\text{mm}$ with relative permittivity $\epsilon_r = 4.2$. The antenna is fed using microstripline feeding because of its simplicity and it can be simultaneously fabricated along with the antenna element. The radius of this antenna is calculated using the equation (1) [12].

$$a = \frac{K}{\left[1 + (2h / \pi \epsilon_r k) \{ \ln(\pi k / 2h) + 1.7726 \} \right]^{-1/2}} \quad (1)$$

where,

$$K = \frac{8.794}{f \epsilon_r^{1/2}} \quad \text{and} \quad a_e = a \left\{ 1 + \frac{2h}{\pi \epsilon_r a \left[\ln\left(\frac{\pi a}{2h}\right) + 1.7726 \right]} \right\}^{1/2}$$

Figure (1) shows the top view geometry of conventional monopole circular microstrip antenna (CMCMSA) in which W_f and L_f are width and length of microstrip feed line respectively.

Figure (2) shows graph of return loss versus frequency of CMCMSA for both simulated and measured. Further figure it is seen that the antenna resonates at 1.99 GHz and 2.0 GHz when simulated and measured respectively.

Figure (3) shows the top view of geometry of TMCMSAWB. This antenna is having the same basic design as that of CMCMSA as shown in figure 1. The radius of the patch and dimensions of microstripline feed are remains same. The conventional monopole CMSA has been modified into TMCMSAWB by adding two identical slots placed on either side of feed axis with a fixed dimensions and the outward stub placed on left side of the patch. The dimensions of the stub width W_s is fixed where as its length are varied from $L_{LS}=0.257\text{cm}$ to 1.057 cm and $L_{US}=0.42\text{ cm}$ to 1.22 cm to tune from 1.74 to 1.47 GHz of TMCMSAWB.

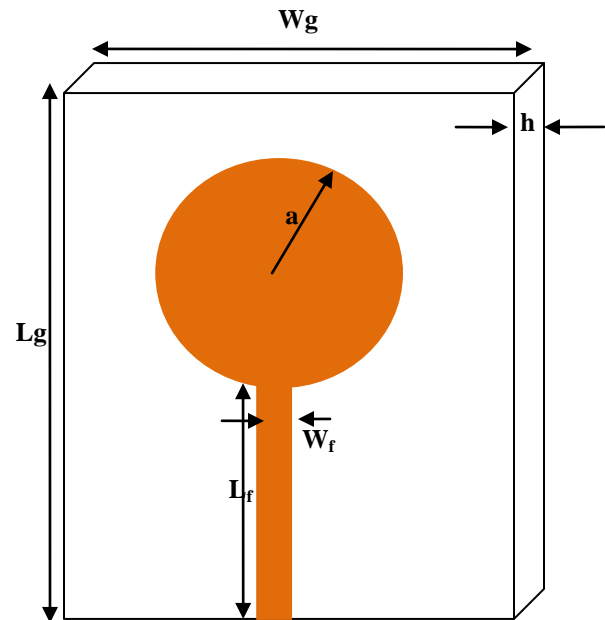


Figure 1. Geometry of CMCMSA

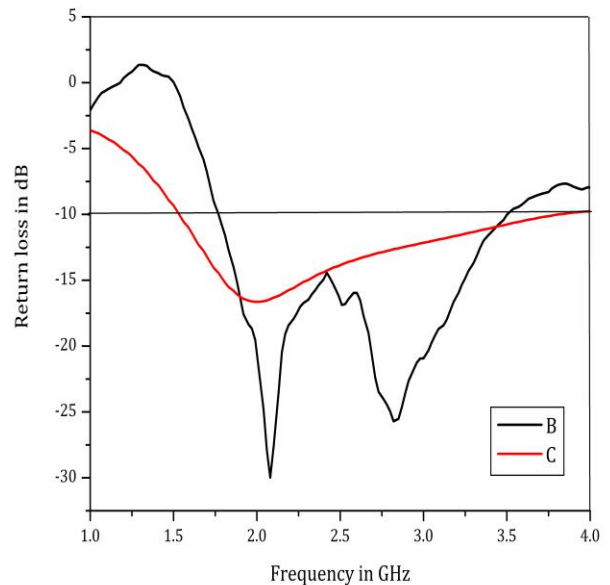


Figure 2. Variation of return loss versus frequency of CMCMSA (simulated and measured)

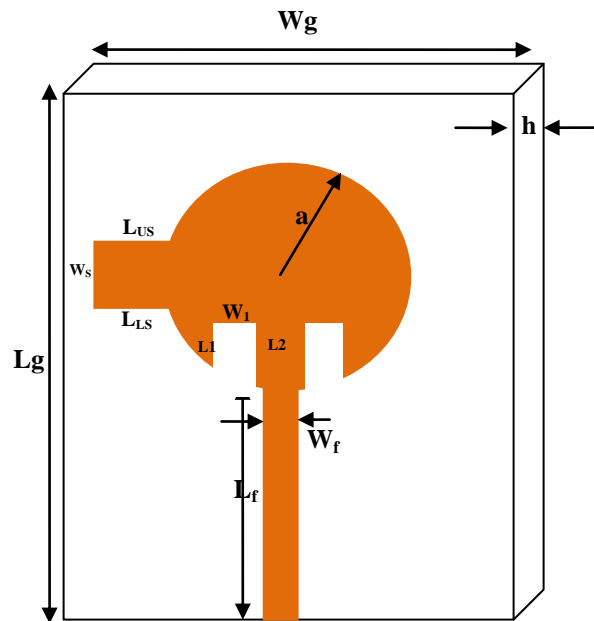


Figure 3. Geometry of proposed TMCMSAWB

Table 1: Design parameter of tunable monopole circular microstrip antenna for wide frequency impedance bandwidth (simulated)

For constant stub width $W_s=0.9\text{cm}$ and with fixed dimensions of two identical slots $L_1=0.446\text{ cm}$, $L_2=0.6\text{cm}$, and $W_1=0.4\text{ cm}$				
Variation of length of stub in cm.	Resonant frequencies in GHz	Return loss in dB	10 dB Bandwidth in GHz	Impedance bandwidth in %
$L_{US} = 0.42\text{ cm}$ & $L_{LS} = 0.257\text{cm}$	$F_{r1} = 1.74$	27.89	2.81	161.58
$L_{US} = 0.62\text{ cm}$ & $L_{LS} = 0.457\text{ cm}$	$F_{r2} = 1.72$	31.43	2.82	164.19
$L_{US} = 0.82\text{ cm}$ & $L_{LS} = 0.657\text{ cm}$	$F_{r3} = 1.65$	26.55	2.81	169.87
$L_{US} = 1.02\text{ cm}$ & $L_{LS} = 0.857\text{ cm}$	$F_{r4} = 1.51$	45.8	2.97	197.00
$L_{US} = 1.22\text{ cm}$ & $L_{LS} = 1.057\text{ cm}$	$F_{r5} = 1.47$	23.4	2.94	200.00

Table 2: Design parameter of tunable monopole circular microstrip antenna for wide frequency impedance bandwidth (measured)

For constant stub width $W_s=0.9\text{cm}$ and with fixed dimensions of two identical slots $L_1=0.446\text{ cm}$, $L_2=0.6\text{cm}$, and $W_1=0.4\text{ cm}$				
Variation of length of stub in cm.	Resonant frequencies in GHz	Return loss in dB	10 dB Bandwidth in GHz	Impedance bandwidth in %
$L_{US} = 0.42\text{ cm}$ & $L_{LS} = 0.257\text{cm}$	$F_{r1} = 1.83$	28.06	1.81	96.9
$L_{US} = 0.62\text{ cm}$ & $L_{LS} = 0.457\text{ cm}$	$F_{r2} = 1.74$	25.34	1.71	98.2
$L_{US} = 0.82\text{ cm}$ & $L_{LS} = 0.657\text{ cm}$	$F_{r3} = 1.65$	24.70	2.04	123
$L_{US} = 1.02\text{ cm}$ & $L_{LS} = 0.857\text{ cm}$	$F_{r4} = 1.55$	24.63	2.02	129
$L_{US} = 1.22\text{ cm}$ & $L_{LS} = 1.057\text{ cm}$	$F_{r5} = 1.46$	35.50	2.40	164

III. RESULTS AND DISCUSSION

Figure 4 and Figure 5 shows the variation of return loss verses frequency of TMCMSAWB when simulated and measured respectively. When an antenna is constructed with two identical slots placed on either side of feed axis with fixed length $L_1= 0.4468$ cm and $L_2= 0.6$ cm with width $W_1=0.4$ cm. The width of left stub $W_s=0.9$ cm can be kept constant and its upper length L_{US} can be varied from 0.42, 0.62, 0.82, 1.02 and 1.22 cm and lower length L_{LS} can be varied from 0.257, 0.457, 0.657, 0.857 and 1.057 cm respectively to tune an antenna from 1.74, 1.72, 1.65, 1.51 and 1.47 GHz of impedance bandwidth in percentages are 161.58, 164.19, 169.87, 197.0 and 200 respectively as shown in Table 1. Table 2 shows measured results in which impedance bandwidths are varies from 98.6 to 164 % and these are in good agreement with simulated values. Figure 6 shows the variation of impedance bandwidth verses frequency in which impedance bandwidth increases when frequency tunes on lower side. The total shift in the frequency from 1.74 to 1.47 GHz is 270 MHz when simulated where as it is 370 MHz when measured having peak gain of 1.9079 dB. All five resonant frequencies have tuned without changing its wideband. In the measured values it is seen that the tuned wide band remains almost constant. The VSWR is less than 2 and shows good matching of antenna. This operating band covers all low frequency wireless communication applications like *GPS (L1 and L2)*, *GSM (1800/1900)*, *Wi-Fi (2.42-2.48 GHz)* *WLAN*, *WiMAX bands (2.3-2.4 GHz, and 3.3-3.4 GHz, 3.4-3.6 GHz, 3.6-3.8 GHz)*, *DCS-1900*, *UMTS-2000*, *LTE-2300/2500*, *FCC ID (2.63 to 2.68GHz) etc.* The impedance band with is calculated using equation (2).

$$\text{Impedance bandwidth (\%)} = \frac{(f_H - f_L)}{f_C} \times 100 \quad (2)$$

Figure 7 shows typical radiation pattern for TMCMSAWB measured at 1.4725 GHz. The patterns are nearly Omni directional in nature both in E and H plane and linearly polarized in both E and H plane [13-17].

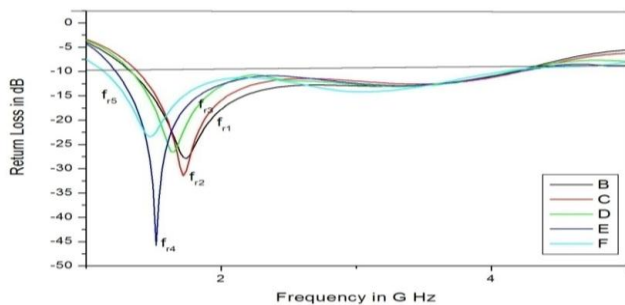


Figure 4. Variation of return loss verses frequency of TMCMSAWB (simulated)

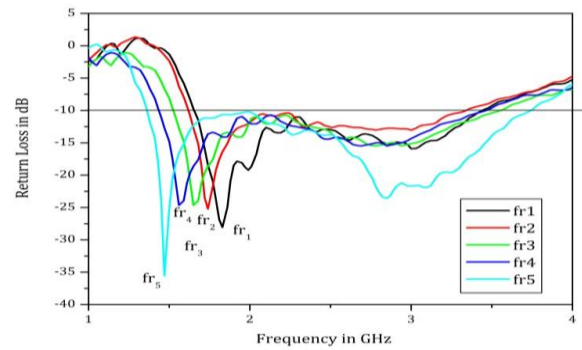


Figure 5. Variation of return loss verses frequency of TMCMSAWB (measured)

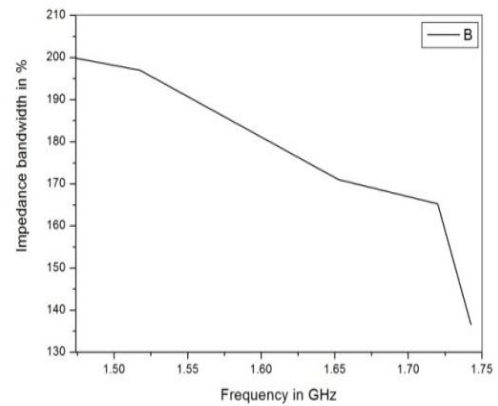


Figure 6. Impedance bandwidth verses frequency of TMCMSAWB

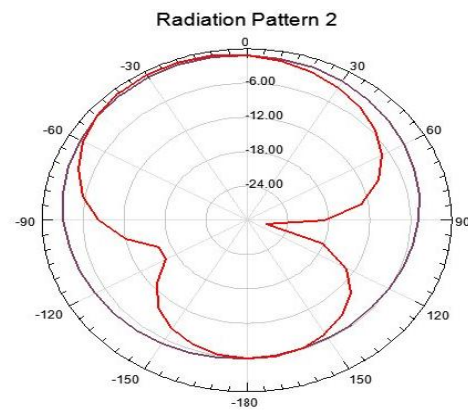


Figure 7: Typical Radiation Pattern TMCMSAWB at 1.4725 GHz

IV. CONCLUSION

The proposed antenna is specifically designed for tuning single wideband having an impedance bandwidth of 200% and this values is in good agreement with measured values of 164 %. This is achieved by designing a novel geometry of antenna proposed in this study. This antenna cover many applications operating at lower microwave frequency range. The new concept of using slots and stub along with the antenna element is very effective in tuning the wide operating band of an antenna. The antenna shows maximum impedance bandwidth of 200 % with a peak gain of 1.9079 dB and finds monopole radiation pattern both in E & H plane. The simulated and experimental results of return loss verses frequency of above is in good agreement with each other . The VSWR is less than 2 for all tuned frequencies with proper matching of antenna . The antenna is simple in its design and uses low cost substrate material. With these features the proposed antenna can be used for the applications such as GPS, GSM, PCS, Wi-Fi, DCS, WiMAX, WLAN and FCC ID etc.

REFERENCES

- [1] Garg, R .P. Bhartia , I . Bhal and A. Ittipiboon, "Microstrip Antenna Design Hand Book", Artech Inc., **2001**.
- [2] A. E. Daniel & G. Kumar, "Tunable dual & triple frequency stub loaded rectangular microstrip antenna (MSA)", Proc. IEEE antennas propagation symposium , **pp.2140-2143, 1995**.
- [3] Balnis C .A , "Antenna theory, Analysis and design", 2nd ed, Wiley, New York, **1997**
- [4] K. P. Ray, S. Nikhil and A. Nair , "Compact Tunable and Dual band Circular Microstrip Antenna for GPS Bluetooth Applications", International Journal of Microwave and Optical Technology, Vol.4, no.4,pp.205-210, **July 2009**.
- [5] L. Tao, J. Xu, H. Li, Y.Hao, S. Huang, M. Lei and K. Bi, "Bandwidth Enhancement of Microstrip Patch Antenna Using Complementary Rhombus Resonator", Wireless Communications and Mobile Computing, Vol. 2018 , Article ID 6352181 , 8 pages , **August 2018**.
- [6] Ruchika Gupta and Mithilesh Kumar, "Bandwidth enhancement of microstrip patch antennas by implementing circular unit cell in circular pattern" 5th International Conference on computational intelligence and communication network, **2013**.
- [7] A. Boutejdar and W. Abd Ellatif, "A novel compact UWB monopole antenna with enhanced bandwidth using triangular defected microstrip structure and stepped cut technique," Microwave and Optical Technology Letters, Vol. 58, no. 6, pp. 1514–1519, **2016**.
- [8] P. Beigi and P. Mohammadi , "Bandwidth enhancement of monopole antenna with DGS for SHF and reconfigurable structure for WiMAX, WLAN and C-band applications" Journal of Instrumentation, Vol.12,pp.1-10,Nov.2017.
- [9] W. Q. Cao and W. Hong, "Bandwidth and gain enhancement for single-fed compact microstrip antenna by loading with parasitical patches," in Proceedings of the 2016 IEEE International Conference on Microwave and Millimeter Wave Technology (ICMMT), pp. **650–652**, Beijing, China, June **2016**.
- [10] A. Nagar, K S. Solanki, "Design and Analysis of Microstrip Patch Antenna", International Journal of Scientific Research in Network security and Communication, Vol.1 , Issue.1 , pp.1-5, Mar-**2013**.
- [11] Ritu Goyal and Y K Jain, "A Review on Bandwidth Enhancement in microstrip Antenna" , International Journal of Computer Sciences and Engineering, Vol.7 , Issue.4 , pp.1196-1200, Apr-**2019** .
- [12] G. Kumar and K.P.Ray,. "Broad Band Microstrip Antennas", Artech House, **2003**
- [13] S.Haykin,"Cognitive radio brain empowered wireless communications," IEEE Journal on Selected Areas in Communications, Vol. 23, no. 2, pp. 201–220, **2005**.
- [14] S.Dey and R. Mittra, "Compact microstrip patch antenna," Microwave and Optical Technology Letters, Vol. 13, no. 1, pp. 12–14, **1996**.
- [15] J. C. Xu, M. Y. Zhao, R. Zhang et al., "A wideband F-shaped microstrip antenna," IEEE Antennas and Wireless Propagation Letters, Vol. 16, pp. 829–832, **2017**.
- [16] J. Xu, L. Tao, R. Zhang, Y. Hao, S. Huang, and K. Bi, "Broadband complementary ring-resonator based terahertz antenna," Optics Express, Vol. 25, no. 15, pp. 17099–17104, **2017**.
- [17] Y. Hao, Q. Wang, X. Gao, S. Huang, and K. Bi, "Frequency tunable slot-coupled dielectric resonators antenna," Journal of Alloys and Compounds, Vol. 702, pp. 664–668, **2017**.

Authors Profile

Mr. Biradar Rajendra pursued Master of Science and Master of Philosophy from Dept of Applied Electronics, Gulbarga University, Kalaburagi, Karnataka in 1988 and 2014 respectively. He is currently pursuing Ph.D and currently working as Associate Professor in Electronics, Karnatak Arts, Science and Commerce College, Bidar, Karnataka since 1990. He has published 03 papers in International Journals Approved by UGC. His main research work focusses on Tunable properties of Microstrip Antenna of different geometry. He has 30 years of teaching experience.



Dr. S. N. Mulgi pursued Master of Science, Master of Philosophy and Ph.D from Gulbarga University, Kalaburagi, Karnataka in 1986, 1987 and 2003 respectively. He is currently working as Professor, Dept of Applied Electronics, Gulbarga University, Kalaburagi, Karnataka, India since 2010. He has guided 12 Ph.D students and published more than 100 papers in National and International Journals. He has chaired many National and International Conferences, Seminars and Symposia. His area of research is Microwave communications, embedded systems etc. He has 30 years of teaching and Research experience.

